

# Storgruppsövning 19/11-13

## Static magnetic fields, kap 6.

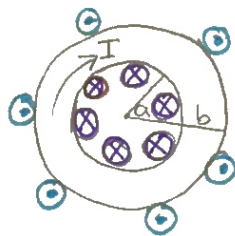
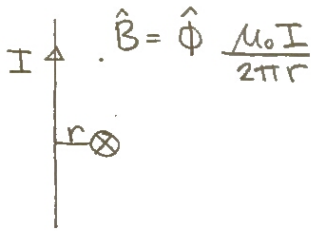
$$\begin{cases} F_e = qE & \text{electric force on } q \text{ in } E \\ F_m = q \mathbf{v} \times \mathbf{B} & \text{magnetic force on moving charge } q \text{ in } \mathbf{B} \end{cases}$$

velocity magnetic flux density

$$\mathbf{F} = F_e + F_m = q(\mathbf{E} + \mathbf{v} \times \mathbf{B}) \quad \text{total electromagnetic force.}$$

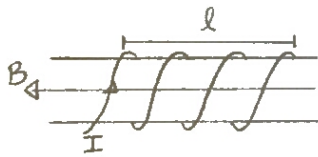
Fundamental postulates of magnetostatic (free space):

$$\begin{cases} \nabla \cdot \mathbf{B} = 0 \implies \oint_S \mathbf{B} \cdot d\mathbf{S} = 0 & \text{law of conservation of magnetic flux} \\ \nabla \times \mathbf{B} = \mu_0 \mathbf{J} \implies \oint_C \mathbf{B} \cdot d\mathbf{l} = \mu_0 I & \text{Ampere's law} \end{cases}$$



$$B = \hat{\phi} \frac{\mu_0 N I}{2\pi r}$$

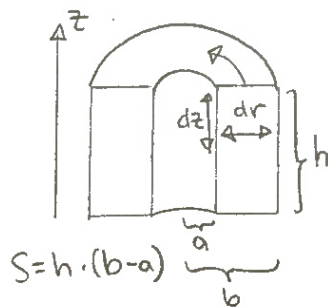
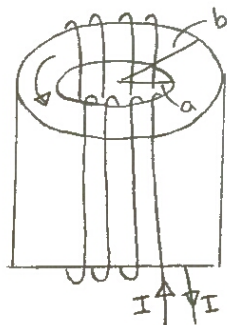
$a < r < b$   
a toroidal-coil



$$B = \mu_0 n I, \quad n = \frac{N}{l} \quad (\text{number of turns per length})$$

### P 6.14

A circular toroid with rectangular cross section. Find the total magnetic flux through its cross section.



$$\Phi = ? = \int_S \mathbf{B} \cdot d\mathbf{S}$$

$$\int \mathbf{B}_\phi \cdot d\mathbf{l} = \mu_0 N I$$

$$\implies B_\phi = \frac{\mu_0 N I}{2\pi r}, \quad a < r < b$$

$$\Phi = \int \mathbf{B}_\phi \cdot \underbrace{d\mathbf{S}}_{dz dr} = (*)$$

$$(*) = \frac{\mu_0 N I}{2\pi} \int_0^h \int_a^b \frac{1}{r} dz dr = \frac{\mu_0 N I h}{2\pi} \ln\left(\frac{b}{a}\right)$$

for. Find the percentage of error if: the flux is found by multiplying the cross-section area by flux density at the mean radius.

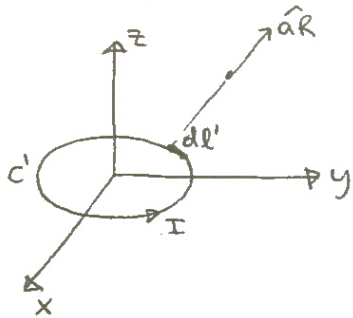
$$B_{\phi}(r = \frac{a+b}{2}) = \frac{\mu_0 N I}{2\pi(\frac{a+b}{2})} = \frac{\mu_0 N I}{\pi(a+b)}$$

$$\Rightarrow \Phi' = B_{\phi}(r = \frac{a+b}{2}) \cdot h(b-a) \Rightarrow \Phi' = \frac{\mu_0 N I h}{\pi} \left( \frac{b-a}{b+a} \right)$$

$$\% \text{ error} = \frac{\Phi' - \Phi}{\Phi} = \left[ \frac{2(b-a)}{(b+a) \ln(b/a)} - 1 \right] \cdot 100$$

The Biot-Savart law:

Gives the magnetic field of a current carrying circuit.



Vector magnetic potential (A)

$$B = \nabla \times A \xrightarrow[\nabla \cdot A = 0]{\text{assume}} \nabla^2 A = -\mu_0 J \Rightarrow A = \frac{\mu_0}{4\pi} \int \frac{J}{R} dV'$$

$$\text{For a closed circuit } A = \frac{\mu_0 I}{4\pi} \oint_C \frac{dl'}{R} \Rightarrow B = \frac{\mu_0 I}{4\pi} \int \frac{dl' \times aR}{R^2}$$

$$B = \oint_{C'} dB, \quad dB = \frac{\mu_0 I}{4\pi} \left( \frac{dl' \times R}{R^3} \right)$$

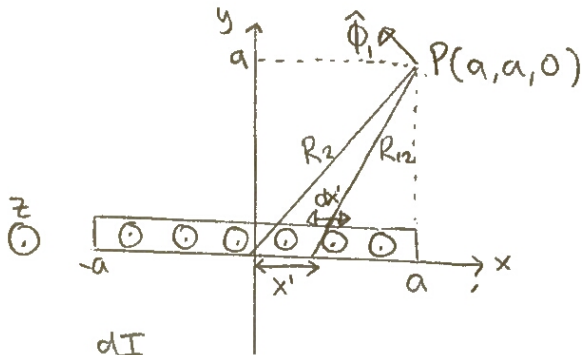
unit vector from source point to the field point

7.2

Biot-Savart law, a very long flat metal strip of width  $2a$ , located in  $x$ - $z$ -plane. The current is distributed uniformly. Find the magnitude and direction of  $B$  at point  $P$ .

$$B(P) = ?$$

$$\text{The current is dist. uniformly} \Rightarrow I = I_0 \hat{z} \Rightarrow \left( J = \frac{I_0}{2a} \hat{z} \right)$$



$$dB = \frac{\mu_0 \overbrace{I_0}^{dI} dx'}{2\pi R_{12}} \hat{\phi}_1$$

$$\begin{cases} R_{12} = R_2 - R_1 = \hat{x}a + \hat{y}a - x'\hat{x} = \hat{x}(a-x') + \hat{y}a \\ R_{12} = \sqrt{(a-x')^2 + a^2} \end{cases}$$

$$\hat{\phi}_1 = \frac{d\mathbf{l}' \times \mathbf{R}_{12}}{R_{12}^3} = \frac{\hat{z} \times \mathbf{R}_{12}}{R_{12}^3} = \frac{\hat{y}(a-x') - \hat{x}(a)}{\sqrt{(a-x')^2 + a^2}}$$

$$dB = \frac{\mu_0 (I_0/2a)}{2\pi} \frac{-\hat{x}a + \hat{y}(a-x')}{(a-x')^2 + a^2} dx' \Rightarrow B = \int_{x'=-a}^a dB$$

$$\Rightarrow dB = \hat{x} dB_x + \hat{y} dB_y \Rightarrow B_x = \int_{x'=-a}^a \frac{-\mu_0 I_0 dx'}{4\pi (a-x')^2 + a^2} =$$

$$= \left\{ \begin{array}{l} a-x' = \xi, d\xi = -dx' \\ x' = -a \Rightarrow \xi = 2a \\ x' = a \Rightarrow \xi = 0 \end{array} \right\} = B_x = \int_{\xi=2a}^0 \frac{\mu_0 I_0 d\xi}{4\pi a (\xi^2 + a^2)} =$$

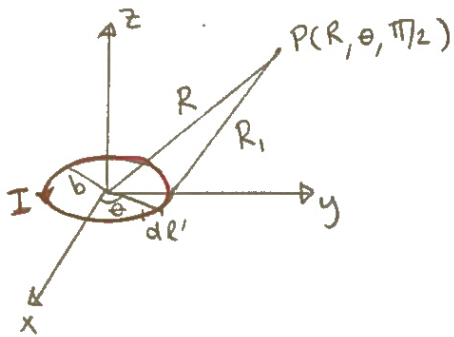
$$= \frac{\mu_0 I_0}{4\pi} \left[ \frac{1}{a} \arctan\left(\frac{\xi}{a}\right) \right]_{2a}^0 = \boxed{-\frac{\mu_0 I_0}{4\pi a} \arctan(2)}$$

$$B_y = \frac{\mu_0 I_0}{4\pi a} \int_{x'=-a}^a \frac{(a-x')}{(a-x')^2 + a^2} dx' = \{p.s.s\} = \frac{-\mu_0 I_0}{4\pi a} \int_{2a}^a \frac{\xi}{\xi^2 + a^2} d\xi =$$

$$= -\frac{\mu_0 I_0}{4\pi a} \left[ \frac{1}{2} \ln(\xi^2 + a^2) \right]_{2a}^a = \frac{\mu_0 I_0}{8\pi a} \ln\left(\frac{4a^2 + a^2}{a^2}\right) = \boxed{\frac{\mu_0 I_0}{8\pi a} \ln(5)}$$

$$\Rightarrow B(P) = B_x + B_y = \frac{\mu_0 I_0}{4\pi a} \left( -\hat{x} \arctan(2) + \hat{y} \frac{\ln(5)}{2} \right)$$

The magnetic dipole: a small circular loop carries a current  $I$ .



$$A = \mu_0 \frac{Im \times \hat{a}_R}{4\pi R^2}, \quad Im = \hat{a}_z \pi b^2 I = \hat{a}_z SI = \hat{a}_z m$$

magnetic dipole moment

$$B = \frac{\mu_0 m}{4\pi R^3} (\hat{a}_R 2\cos\theta + \hat{a}_\theta \sin\theta)$$

### 7.10

A magnetic dipole  $m = \hat{z} m$  is in origin. Find the magnetic flux through the ring.

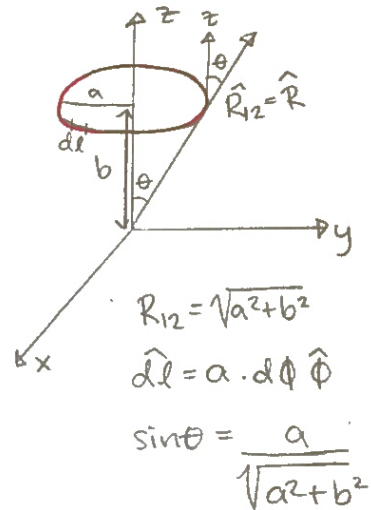
$$\Phi = \int_S B \cdot dS = ? = \int_S (\nabla \times A) \cdot dS = \oint_C A \cdot dl$$

$$A = \mu_0 \frac{Im \times \hat{R}_{1,2}}{4\pi R_{1,2}^2} = \frac{\mu_0 \hat{z} m \times \hat{R}}{4\pi(a^2 + b^2)}$$

$$= \frac{\mu_0}{4\pi(a^2 + b^2)} m \sin\theta \hat{\phi}$$

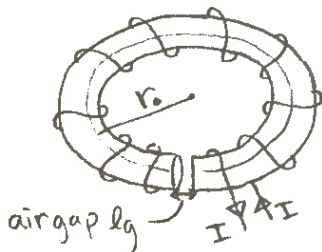
$$\Phi = \oint_C A \cdot dl = \int_{\phi=0}^{2\pi} \frac{\mu_0 m}{4\pi(a^2 + b^2)} \frac{a}{\sqrt{a^2 + b^2}} \hat{\phi} (\hat{\phi} a d\phi) =$$

$$= \frac{\mu_0 m a^2}{2(a^2 + b^2)^{3/2}}$$



### ex 6.10 i boken

Magnetic circuits,  $N$ -turns of wire around ferromagnetic Toroidal-coil. Find  $B$  and  $H$  both in core and in air-gap.



Permeability:  $\mu$   
 mean radius:  $r_0$   
 cross-section of coil:  $a \ll r_0$

for  $T_s \rightarrow$

Neglecting fringing and leakage:  $B_f = B_g = \hat{\Phi} B_f$

$$\rightarrow \begin{cases} H_f = \hat{\Phi} \frac{B_f}{\mu} & \text{magnetic flux intensity in coil} \\ H_g = \hat{\Phi} \frac{B_f}{\mu_0} & \text{magnetic flux intensity in airgap} \end{cases}$$

Ampere's law:

$$\oint H \cdot dl = NI_0 \rightarrow \frac{B_f}{\mu} (2\pi r_0 - l_g) + \frac{B_f}{\mu_0} \cdot l_g = NI_0$$

$$\rightarrow B_f = \hat{\Phi} \frac{\mu \mu_0 NI_0}{\mu_0 (2\pi r_0 - l_g) + \mu l_g}$$

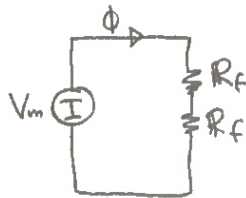
Assume  $B$  constant  $\implies \Phi = B S = \frac{NI_0}{\frac{2\pi r_0 - l_g}{S} + \frac{l_g}{S \mu_0}}$

$\Phi = \frac{V_m}{R_f + R_g}$  — reluctance

magneto motive force.

$$R_f = \frac{2\pi r_0 - l_g}{\mu S}, \quad R_g = \frac{l_g}{S \mu_0}$$

$$I = \frac{V_e}{R_f + R_g}$$





# Storgruppsövning 19/11-13 em.

## Resistansberäkningar, övre och undre gräns

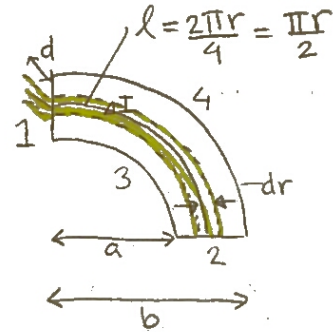
6.16  
 quarter disk, ( $\sigma$  = conductivity)  
 $d$  = thickness

a) Calculate  $R_{12}$  (between electrodes 1 & 2)

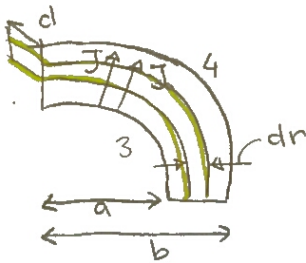
$$dG = \frac{\sigma S}{l} = \frac{\sigma (dr \cdot d)}{\pi r / 2} = \frac{2\sigma d}{\pi r} dr$$

$$G_{12} = \int_{r=a}^b dG = \int_a^b \frac{2\sigma d}{\pi r} dr = \frac{2\sigma d}{\pi} \ln\left(\frac{b}{a}\right)$$

$$\Rightarrow R_{12} = \frac{1}{G_{12}} = \frac{\pi}{2\sigma d \ln(b/a)} \quad \text{parallellkoppling}$$



b)



$$dR = \frac{l}{\sigma S} = \frac{dr}{\sigma \cdot \pi r d / 2} = \frac{2}{\sigma \pi r d} dr$$

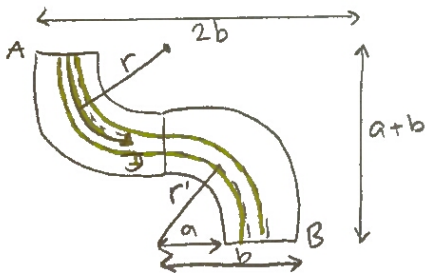
$$S = \frac{\pi}{2} r d$$

$$R_{34} = \int_{r=a}^b dR = \int_a^b \frac{2}{\sigma \pi r d} dr = \frac{2}{\sigma \pi d} \ln\left(\frac{b}{a}\right) \quad \text{seriekoppling}$$

$$R_{12} \cdot R_{34} = \frac{\pi}{2\sigma d \ln(b/a)} \cdot \frac{2 \ln(b/a)}{\sigma \pi d} = \left(\frac{1}{\sigma d}\right)^2$$

6.17

A thin plate, has thickness  $d=0,1\text{mm}$  and conductivity  $\sigma$ .  
 Find upper and lower bounds for  $R_{AB}$  if  $2a=b$ .



- Upper bound: assume current tubes.

$$dG = \frac{\sigma S}{l}, \quad \begin{cases} l = \frac{\pi}{2} r + \frac{\pi}{2} (a+b-r) \\ S = d \cdot dr \end{cases}$$

forts. →

# Storgruppsövning 19/11-13 em.

## Resistansberäkningar, övre och undre gräns

6.16

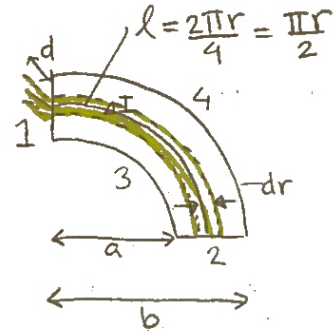
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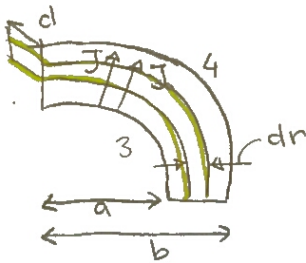
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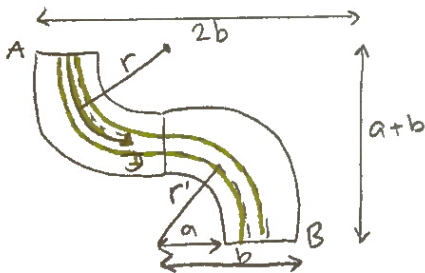
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$$R_{12} \cdot R_{34} = \frac{\pi}{2\sigma d \ln(b/a)} \cdot \frac{2 \ln(b/a)}{\sigma \pi d} = \left(\frac{1}{\sigma d}\right)^2$$

6.17

A thin plate, has thickness  $d=0,1\text{mm}$  and conductivity  $\sigma$ .  
 Find upper and lower bounds for  $R_{AB}$  if  $2a=b$ .



- Upper bound: assume current tubes.

$$dG = \frac{\sigma S}{l}, \quad \begin{cases} l = \frac{\pi}{2} r + \frac{\pi}{2} (a+b-r) \\ S = d \cdot dr \end{cases}$$

forts. →

$$\rightarrow dG = \frac{\delta d z}{\pi(a+b)} dr$$

$$\rightarrow G = \int_{r=a}^b dG = \int_a^b \frac{2\delta d}{\pi(a+b)} dr = \frac{2\delta d(b-a)}{\pi(a+b)} = \{b=2a\} = \frac{2\delta d}{3}$$

$$\rightarrow R = \frac{3\pi}{2\delta d} = 0,471 \Omega$$

lower bound: assume an equipotential surface as real-line

$$R^2 = 2R_{12} = 2 \cdot \frac{\pi}{2\delta d \ln(b/a)} = \frac{\pi}{\delta d \ln(2)} = 0,453 \Omega$$

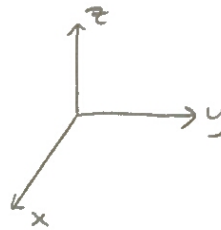
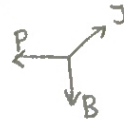
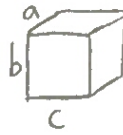
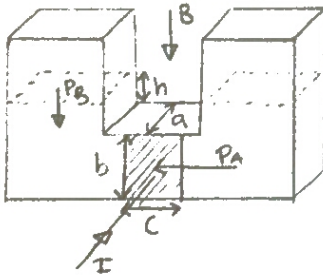
↑  
from 6.16

$$\rightarrow 0,453 < \text{actual } R_{AB} < 0,471$$

7.8

(u-tube) in the figure is filled with a conductor fluid, mass density  $\eta$ .

Find height difference in two legs.



$$J_0 = \frac{J}{bc}$$

$$F_m = qV \times B = \int \Delta V \mathbb{V} \times B \Rightarrow \frac{F}{\Delta V} = \int \mathbb{V} \times B$$

$$\begin{cases} \mathbb{J} = -\hat{x} J_0 \\ \mathbb{B} = -B_0 \hat{z} \end{cases}$$

$$f = q/\Delta V \Rightarrow q = f\Delta V$$

$$\mathbb{J} = f\mathbb{V} \quad \text{convection current}$$

$$\Rightarrow \frac{F}{\Delta V} = \mathbb{J} \times \mathbb{B} = -J_0 B_0 \hat{y} \left( \frac{N}{m^3} \right) \quad \left( (-\hat{x} J_0) \times (-B_0 \hat{z}) \right)$$

$$F_A = \frac{F}{\Delta V} \cdot abc = J_0 B_0 abc \quad (\text{the force in cubic region})$$

$$P_A = \frac{F_A}{ab} \quad (\text{the force acts on the shaded area, cause the pressure } P_A)$$

$$P_A = \frac{J_0 B_0 abc}{ab} = J_0 B_0 c$$

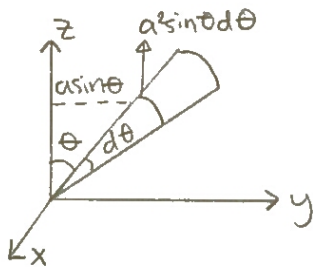
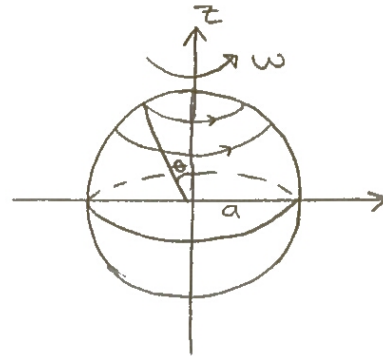


$$P_B = \underbrace{\rho}_{\text{mass density}} g h = J_0 B_0 C \implies h = \frac{J_0 B_0 C}{\rho g}$$

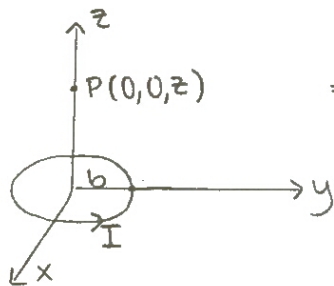
7.7  
 Biot-Savart law, a metal sphere of radius  $a$  with charge  $Q$ ,  
 distributed uniformly  
 - angular velocity  $\omega$   
 - Find  $B$  in center!

$$\omega = \frac{d\phi}{dt}, \quad \rho_s = \frac{Q}{4\pi a^2}$$

$$dq = \rho_s ds = \rho_s ds_R = \rho_s a^2 \sin\theta d\theta d\phi$$



$$di = \frac{dq}{dt} = \rho_s a^2 \sin\theta d\theta \frac{d\phi}{dt} = \rho_s a^2 \sin\theta \omega d\theta$$



$$\implies B(P) = \hat{z} \frac{\mu_0 I b^2}{2(z^2 + b^2)^{3/2}}$$

$$\left\{ \begin{array}{l} I = di \\ b = a \sin\theta \\ z = a \cos\theta \\ z^2 + b^2 = a^2 \end{array} \right.$$

$$\implies dB = \hat{z} \frac{\mu_0 di (a \sin\theta)^2}{2a^3} =$$

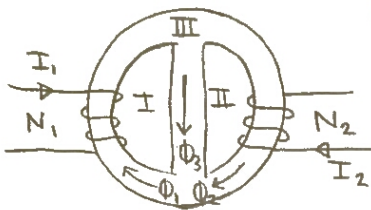
$$= \hat{z} \frac{\mu_0 Q \omega}{8\pi a} \sin^3\theta d\theta$$

$$B = \int_{\theta=0}^{\pi} dB = \hat{z} \frac{\mu_0 Q \omega}{6\pi a}$$

8.5

$$\text{Rules: } \sum_j N_j I_j = \sum_k \mathcal{R}_k \Phi_k \text{ around a close path in a magnetic circuit.}$$

$$\sum_j \Phi_j = 0 \text{ in a junction}$$

Iron ring ( $a = 7.5 \text{ cm}$ ) and ( $A_1 = 1.2 \text{ cm}^2$ ) $(A_3 = 0.8 \text{ cm}^2)$  $(N_1 = 160 \text{ turns})$   
 $(N_2 = 120 \text{ turns})$  $I_1 = I_2 = 2 \text{ mA}$ a) Calculate the flux through the bridge ( $\Phi_3$ )

$$\begin{cases} \text{I: } \mathcal{R}_1 \Phi_1 + \mathcal{R}_3 \Phi_3 = N_1 I_1 \\ \text{II: } \mathcal{R}_2 \Phi_2 - \mathcal{R}_3 \Phi_3 = N_2 I_2 \\ \text{III: } \Phi_1 = \Phi_2 + \Phi_3 \end{cases}$$

$$\mathcal{R}_1 = \mathcal{R}_2 = \frac{l_1}{\mu A_1} = \frac{\pi a}{\mu A_1}$$

$$\mathcal{R}_3 = \frac{l_3}{\mu A_3} = \frac{2a}{\mu A_3}$$

In matrix-form:

$$\begin{bmatrix} \mathcal{R}_1 + \mathcal{R}_3 & -\mathcal{R}_3 \\ -\mathcal{R}_3 & \mathcal{R}_1 + \mathcal{R}_3 \end{bmatrix} \begin{bmatrix} \Phi_1 \\ \Phi_2 \end{bmatrix} = \begin{bmatrix} N_1 I_1 \\ N_2 I_2 \end{bmatrix} \Rightarrow \Phi_3 = 2,639 \cdot 10^{-9} \text{ (wb)}$$

b) we assume  $I_2 = 0$ , Find  $I_1$  in order to have  $\Phi_3 = 60 \cdot 10^{-6} \text{ wb}$   
use magnetization chart for iron

$$\Phi_3 = 60 \cdot 10^{-6} \Rightarrow \Phi_3 = B_3 A_3 \Rightarrow B_3 = \frac{\Phi_3}{A_3} = \frac{60 \cdot 10^{-6}}{0,8 \cdot 10^{-4}} = 0,75 \text{ (T)}$$

use chart for iron:  $H_3 = 4200 \text{ (A/m)}$ 

$$\oint H \cdot dl = I \xrightarrow{\text{in loop II}} H_3 \cdot 2a - H_2 \cdot \pi a = 0 \Rightarrow H_2 = 2800 \text{ (A/m)}$$

use chart  $\Rightarrow B_2 = 0,65 \text{ (T)}$ ,  $B_2 = \Phi_2 / A_2 \Rightarrow \Phi_2 = 78 \cdot 10^{-6} \text{ wb}$ in junction III:  $\Phi_1 = \Phi_2 + \Phi_3 \Rightarrow \Phi_1 = 138 \cdot 10^{-6} \text{ wb}$ 

$$\Rightarrow B_1 = \frac{\Phi_1}{A_1} = 1,15 \text{ (T)}, \text{ chart } \Rightarrow H_1 = 20000 \text{ (A/m)}$$

facts  $\rightarrow$

$$\text{loop I} \Rightarrow \oint \mathbf{H} \cdot d\mathbf{l} = I \Rightarrow H_1 \cdot \pi a + H_3 \cdot 2a = NI_1$$

$$\Rightarrow I_1 = \frac{H_1 \cdot \pi a + H_3 \cdot 2a}{N} = 33,6 \text{ A}$$